

## UNIVERSITY OF RUHUNA

## **Faculty of Engineering**

End-Semester 7 Examination in Engineering: May 2023

Module Number: CE7252

Module Name: Ground Improvement Techniques

[Three Hours]

[Answer all questions]
[Each question carries FIFTEEN marks]

Q1. A road is to be constructed on a low lying area underlain by very soft clay of thickness 8.0 m. Dense sand is found below the very soft clay layer. A cross section of the sub surface soil profile is shown in Figure Q1.1.

It was decided to raise the subgrade level by 5.0 m in order to prevent frequent flooding in the area. To compensate the pavement load, traffic load and consolidation settlement, additional 3.0 m thick soil fill will be placed on the subgrade level as shown in Figure Q1.1. The ground water table is found to be at the existing ground level.

It was decided to improve the sub soil by installing Gravel Compaction Piles (GCP) up to a depth of 8.0 m prior to start the embankment construction. The diameter of the GCP is 0.7 m. It is proposed to place GCP at 1.2 m spacing in square pattern. The unit weight and friction angle of the material in the GCP is 22 kN/m³ and 36° respectively.

Bulk unit weight of very soft clay, dense sand and fill material can be taken as  $15.0\,\mathrm{kN/m^3}$ ,  $18.0\,\mathrm{kN/m^3}$  and  $20.0\,\mathrm{kN/m^3}$  respectively. Laboratory test results revealed that coefficient of consolidation of very soft clay in vertical and horizontal directions are  $1.5\,\mathrm{m^2/year}$  and  $6.0\,\mathrm{m^2/year}$  respectively. The compression index, initial void ratio and undrained shear strength of very soft clay are 0.6,  $1.2\,\mathrm{and}\,5\,\mathrm{kN/m^2}$  respectively.

You may use following equations with usual notations for calculations.

$$a_s = 0.785 \left(\frac{D}{s}\right)^2 \text{ for square pattern}$$

$$D_e = 1.13S \text{ for square pattern}$$

$$\mu_c = \frac{1}{1 + (n-1)a_s}$$

$$\mu_s = \frac{n}{1 + (n-1)a_s}$$

$$n^* = \frac{D_e}{D'}$$

$$U = 1 - (1 - U_v)(1 - U_h)$$

$$T_h = \frac{C_h t}{D_e^2}$$

a) Briefly explain densification and solidification concepts used in ground improvement techniques. List 2 methods under each category.

[2.0 Marks]

b) What are the advantages of Gravel Compaction Pile (GCP) technique over preloading technique.

[1.0 Marks]

c) Why is it important to use singly graded aggregates for GCP rather than well gradated aggregates?

[1.0 Marks]

d) Due to highly variable nature of the sub surface soil profile, list 2 methods to make sure that all GCPs were installed up to the dense sand layer.

[1.0 Marks]

e) After installation of GCPs, Dynamic Cone Penetration Test (DCPT) is used to verify the compaction of the granular material in the GCP. Briefly describe why DCPT is more popular over Standard Penetration Test (SPT) to determine the compaction of granular material within the GCP?

[1.0 Marks]

f) If stress concentration ratio (n) is 5, compute the settlement reduction ratio due to proposed ground improvement technique.

[5.0 Marks]

g) The effective drainage area of the GCP is reduced due to smear effect during operation. If drainage area of GCP is reduced by 80% of the original area, estimate the time required for 90% of the primary consolidation by neglecting the effect of vertical drainage. The information provided in Table Q1.1 and Figure Q1.2 may useful in the calculations.

[3.0 Marks]

h) Suggest a suitable method to minimize the reduction of drainage area of GCP due to smear effect during the operation?

[1.0 Marks]

Q2. An expressway is to be constructed on a marshy land consists of 4.0 m thick soft sandy clay layer. Borehole investigation revealed that completely weathered rock is below the soft sandy clay layer. According to the plan and profile of the expressway, subgrade is 4.0 m above the existing ground level. The water table is at the existing ground surface.

It is suggested to adopt preloading technique to improve the soft sandy clay layer and embankment finished level is decided keep 3.0 m above the subgrade level. A gravel mat together with geotextiles are placed over the soft sandy clay layer before placing the embankment fill. Cross section of the proposed embankment is shown in Figure Q2.1.

A series of laboratory tests were conducted to find the index properties and the compressibility characteristics of the soft sandy clay and the results are illustrated in Table Q2.1. The bulk unit weight of the fill material can be taken as  $20 \, \text{kN/m}^3$ . Assume that unit weight of gravel mat and embankment material is same. The unit weight of water can be taken as  $9.81 \, \text{kN/m}^3$ . The information provided in Table Q1.1 may useful in the calculations.

Note:- You may consider the variation of the thickness of the clay layer in different stages. But consider the unit weight to be the same.

a) Briefly explain the concept of "Preloading" with suitable sketches.

[1.0 Marks]

b) List 2 advantages of placing a gravel mat together with a geotextile over the clay layer before placing the fill?

[1.0 Marks]

c) As first step, it is proposed to place 3.5 m thick compacted fill on the soft sandy clay layer. If filling rate is 0.5 m/week, what would be the degree of consolidation at the end of stage 1 filling?

[1.5 Marks]

d) The second stage of filling is started after the end of stage 1 filling and fill thickness is 4.0 m. If filling rate is 0.5 m/week, what would be the overall degree of consolidation at the end of stage 2 filling?

[5.0 Marks]

e) If preloading period is 120 days, what would be the overall degree of consolidation at the end of preloading period?

[3.5 Marks]

f) What would be the expected primary consolidation settlement at the end of preloading period?

[1.0 Marks]

- g) What would be the expected removable fill height after the end of preloading? [1.0 Marks]
- h) If pavement and traffic load is 25 kN/m², what would be the expected Over Consolidation Ratio (OCR) of the soft sandy clay layer after construction of the road?

[1.0 Marks]

Q3. A four lane highway was constructed over a low lying area underlain with 6.0 m thick soft clay layer. Dense sand is found under the clay layer. As this area is frequently subjected to flooding, it was decided to raise the elevation of the subgrade level by 4.0 m. In order to compensate the dead and live load of the highway, and consolidation settlement, an additional soil fill of 2.5 m was placed over the embankment.

Compressibility characteristics of soft clay together with other index properties are shown in Table Q3.1. The bulk unit weight of fill material can be taken as  $20 \text{ kN/m}^3$ . The ground water table is found to be at the existing ground level.

In order to accelerate the consolidation of soft clay layer due to soil fill, Prefabricated Vertical Drains (PVD) were installed in triangular pattern up to a depth of 6.0 m. A gravel mat together with a geotextile was placed over the soft clay layer. The cross sectional dimensions of  $100 \text{ mm} \times 4 \text{ mm}$  and  $120 \text{ mm} \times 60 \text{ mm}$  are used for PVD and mandrel respectively. The discharge capacity of the drain is given as  $900 \text{ m}^3/\text{year}$ . The unit weight of water can be taken as  $9.81 \text{ kN/m}^3$ .

The following equations with usual notations and information provided in Table Q1.1 may useful in the calculations.

$$U_h = 1 - exp\left[\frac{-8T_h}{F}\right]$$

$$T_h = \frac{C_h t}{D_e^2}$$

$$F = F_{(n)} + F_s + F_r$$

$$F_{(n)} = \ln\left[\frac{D_e}{d_w}\right] - \frac{3}{4}$$

$$F_s = \left[\left(\frac{k_h}{k_s}\right) - 1\right] \ln\left(\frac{d_s}{d_w}\right)$$

$$F_r = \frac{2}{3}\pi L^2 \left(\frac{k_h}{q_w}\right)$$

$$D_e = 1.13S \text{ for square pattern}$$

$$D_e = 1.05S \text{ for triangular pattern}$$

$$d_s = 2d_m$$

$$C_h = \left(\frac{k_h}{k_v}\right) C_v$$

$$U = 1 - (1 - U_h)(1 - U_v)$$

a) What are the functions of synthetic filter jacket and plastic core in Prefabricated Vertical Drains (PVDs)?

[2.0 Marks]

b) "With the installation of PVD, settlement of the soft ground can be reduced". Do you agree with this statement? Justify your answer with a suitable sketch.

[1.0 Marks]

c) "Vertical drains increase the undrained shear strength of soft soil due to consolidation". Do you agree with this statement? Justify your answer.

[1.0 Marks]

d) Why is it important to do "Depth check" before installation of PVD in the field? [1.0 Marks]

e) Assuming that soft clay is normally consolidated, what would be the expected primary consolidation settlement of the clay layer due to embankment load after installation of PVD at 1.0 m spacing?

[1.5 Marks]

- f) By neglecting the vertical drainage, what would be the expected time to achieve 95% degree of consolidation due to embankment load after installation of PVD?

  [7.0 Marks]
- g) In order to achieve the required degree of consolidation within 3 months, it was suggested to further reduce the PVD spacing. As a junior geotechnical engineer in the project, would you agree with this decision? Justify your answer and suggest an alternative method to reduce the consolidation period.

[1.5 Marks]

- Q4. A large land area was acquired to the Colombo city through the Port city development project and offshore sand was pumped to fill the reclaimed area. Thickness of the loose sandy soil deposit at the reclaimed area is about 6.0 10.0 m. Since relative density of the loose sandy soil deposit is 20%, dynamic compaction and vibroflotation techniques were proposed to improve the subsurface.
  - a) When the loose sandy soil thickness is less than 6.0 m, dynamic compaction technique is proposed to improve the subsurface. It was decided to use 15 ton tamper falling from a height of 10 m. The crane employed is 100 ton capacity type. Assume that energy loss during tamping is about 20 % and the compaction energy required to improve loose sandy deposit is 25 tm/m³.

i) Briefly explain why Dynamic compaction technique is not suitable to improve very soft clay?

[1.0 Marks]

ii) Briefly explain with neat sketches mechanism and principle of Dynamic Compaction Technique.

[1.5 Marks]

iii) Design a suitable dynamic compaction programme in order to improve the loose sandy soil deposit. Specify the maximum possible depth of improvement, spacing, number of blows per phase and number of phases with a suitable sketch. You may use the following equation with usual notations.

 $D = 0.5\sqrt{WH}$ 

[2.5 Marks]

- b) Vibroflotation technique is proposed to adopt when the loose sandy soil deposit is greater than 6.0 m.
  - i) Briefly describe the vibroflotation technique under wet process with suitable sketches

[2.0 Marks]

ii) What is the difference between vibro-compaction and vibro-replacement.

[1.0 Marks]

iii) Estimate the suitable probe spacing in triangular pattern under 30 hp vibroflot unit, to achieve 90 % relative density using the D'Appolonia's method. The information provided in Figure Q4.1 may useful in the calculations.

[2.0 Marks]

- c) It was proposed to use soil-cement columns to support the underground sewer pipes in the Port city development area.
  - i) What are the Primary cementitious products in the soil-cement mixing technique.

[1.5 Marks]

ii) What is Pozzolanic Reaction in soil-cement mixing technique.

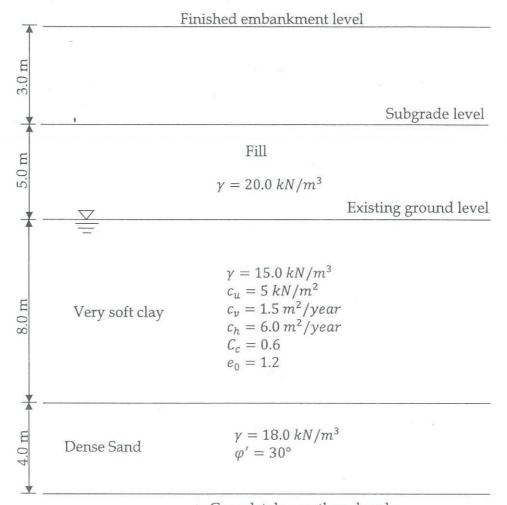
[1.0 Marks]

iii) Briefly explain how the "Curing Period" affect on the rate of shear strength gain in soil-cement mixing.

[1.0 Marks]

iv) Briefly describe the "Wet Jet Mixing Method" which is used to stabilize soft clay.

[1.5 Marks]



Completely weathered rock

Figure Q1.1 Cross section of the road embankment with sub surface soil profile

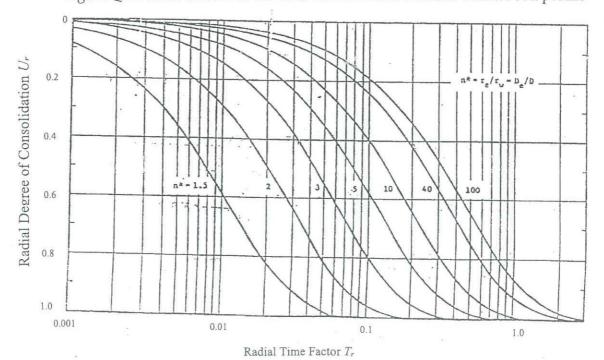


Figure Q1.2 Variation of degree of consolidation in radial direction with time factor

Table Q1.1 – Variation of  $T_v$  with U

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13       0.0133       64       0.329         14       0.0154       65       0.304         15       0.0177       66       0.352         16       0.0201       67       0.364         17       0.0227       68       0.377         18       0.0254       69       0.390         19       0.0283       70       0.403         20       0.0314       71       0.417         21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84	)					0.318
14       0.0154       65       0.304         15       0.0177       66       0.352         16       0.0201       67       0.364         17       0.0227       68       0.377         18       0.0254       69       0.390         19       0.0283       70       0.403         20       0.0314       71       0.417         21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85						0.329
15						0.304
16		2-0	ĕ			0.352
17       0.0227       68       0.377         18       0.0254       69       0.390         19       0.0283       70       0.403         20       0.0314       71       0.417         21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>0.364</td></td<>						0.364
18       0.0254       69       0.390         19       0.0283       70       0.403         20       0.0314       71       0.417         21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       3       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113						0.377
19				69		0.390
20       0.0314       71       0.417         21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0						0.403
21       0.0346       72       0.431         22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.						0.417
22       0.0380       73       0.446         23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         43       0.145       94       1.0					-	0.431
23       0.0415       74       0.461         24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.05				73		0.446
24       0.0452       75       0.477         25       0.0491       76       0.493         26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129	The second secon			74		0.461
25		0.0452		. 75		0.477
26       0.0531       77       0.511         27       0.0572       78       0.529         28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336 </td <td></td> <td>0.0491</td> <td></td> <td>76</td> <td></td> <td></td>		0.0491		76		
28		0.0531		77		
28       0.0615       79       0.547         29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336         47       0.173       98       1.500         48       0.181       99       1.781 <td>27</td> <td>0.0572</td> <td></td> <td>78</td> <td></td> <td></td>	27	0.0572		78		
29       0.0660       80       0.567         30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336         47       0.173       98       1.500         48       0.181       99       1.781         49       0.188       100       ∞	1	0.0615		79		4
30       0.0707       81       0.588         31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336         47       0.173       98       1.500         48       0.181       99       1.781         49       0.188       100       ∞		0.0660		80		1
31       0.0754       82       0.610         32       0.0803       83       0.633         33       0.0855       84       0.658         34       0.0907       85       0.684         35       0.0962       86       0.712         36       0.102       87       0.742         37       0.107       88       0.774         38       0.113       89       0.809         39       0.119       90       0.848         40       0.126       91       0.891         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336         47       0.173       98       1.500         48       0.181       99       1.781         49       0.188       100       ∞		0.0707		81		The second secon
33	31	0.0754				
34     0.0907     85     0.684       35     0.0962     86     0.712       36     0.102     87     0.742       37     0.107     88     0.774       38     0.113     89     0.809       39     0.119     90     0.848       40     0.126     91     0.891       41     0.132     92     0.938       42     0.138     93     0.993       43     0.145     94     1.055       44     0.152     95     1.129       45     0.159     96     1.219       46     0.166     97     1.336       47     0.173     98     1.500       48     0.181     99     1.781       49     0.188     100     ∞	32	0.0803				
35 0.0962 86 0.712 36 0.102 87 0.742 37 0.107 88 0.774 38 0.113 89 0.809 39 0.119 90 0.848 40 0.126 91 0.891 41 0.132 92 0.938 42 0.138 93 0.993 43 0.145 94 1.055 44 0.152 95 1.129 45 0.159 96 1.219 46 0.166 97 1.336 47 0.173 98 1.500 48 0.181 99 1.781 49 0.188 100 ∞	33	0.0855				
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39       0.126       91       0.891         40       0.126       91       0.938         41       0.132       92       0.938         42       0.138       93       0.993         43       0.145       94       1.055         44       0.152       95       1.129         45       0.159       96       1.219         46       0.166       97       1.336         47       0.173       98       1.500         48       0.181       99       1.781         49       0.188       100       \infty	38					
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43 0.145 94 1.055 44 0.152 95 1.129 45 0.159 96 1.219 46 0.166 97 1.336 47 0.173 98 1.500 48 0.181 99 1.781 49 0.188 100						경영 경영 생활 시간 경기
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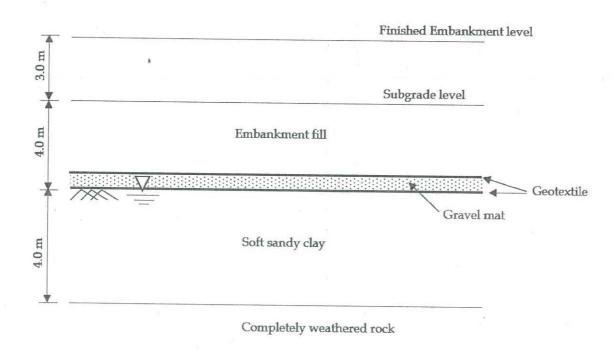


Figure Q2.1 Cross section of the embankment with sub surface soil profile

Table Q2.1 - Properties of soft sandy clay

Saturated unit weight $\gamma_{sat}$	$15.0  \text{kN/m}^3$	
Coefficient of consolidation $C_{\nu}$	8.0 m <sup>2</sup> /year	
Modified Compression index $C'_c$	0.25	
Undrained shear strength $c_u$	20.0 kN/m <sup>2</sup>	

Table Q3.1 - Properties of soft clay

Saturated unit weight	15.0 kN/m <sup>3</sup>	
Coefficient of consolidation in vertical direction	2.0 m <sup>2</sup> /year	
Coefficient of consolidation in horizontal direction	4.0 m <sup>2</sup> /year	
Compression index	0.6	
Initial void ratio	1.2	
Coefficient of horizontal permeability	1 x 10-7 cm/s	

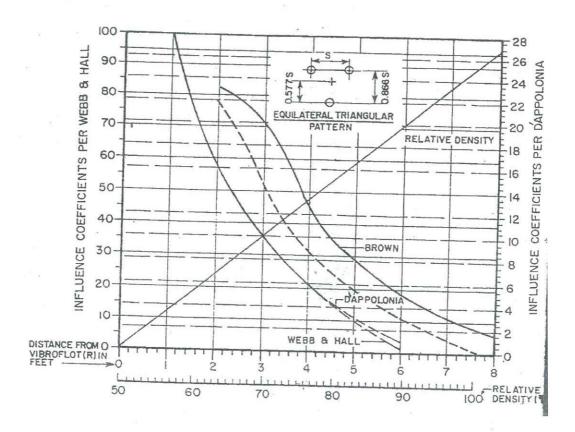


Figure Q4.1 - Area pattern design chart (D'Appolonia's chart)