



UNIVERSITY OF RUHUNA

Faculty of Engineering

End-Semester 4 Examination in Engineering: February 2020

Module Number: CE4302

Module Name: Design of Concrete Structures I

[Three Hours]

[Answer all questions, all questions carry twelve marks each.]

EC2: SLS EN 1992-1-1:2012(EN1992-1-1:2004) is provided, BS 8110 provided

(All symbols used in the paper have their usual meaning unless otherwise stated)

- Q1. a) Rectangular beam 250 mm × 500 mm (see Fig. Q1 (a)) with an effective depth (d) of 452.5 mm is reinforced with five Nos. of 25mm diameter high yield steel bars at the bottom and 02 Nos. of 20 mm diameter high yield steel bars at the top. Take $f_{ck} = 25 \text{ N/mm}^2$, $f_{yk} = 500 \text{ N/mm}^2$ and $E_s = 200 \text{ kN/mm}^2$ and calculate the sagging moment carrying capacity of the section. Assume effective depth to top reinforcement (d') equals to 47.5 mm. You may ignore the contribution from the top reinforcement in the calculation of capacity of the beam. [5 Marks]
- b) Composite concrete slab of 125mm is cast at the top of the beam described in the Q1. a) above and that 950 mm slab width is effectively contributing to the beam flange action as shown in Fig Q1 (b) when the beam is subjected to sagging moment.
- i) Calculate the new sagging moment capacity of the section considering the flange action of the slab. [4 Marks]
- ii) Calculate the reinforcement requirement to support the moment capacity found in Q1 (b) i) without the flange action (i.e. considering section as rectangular beam 250 mm wide and 500 mm deep). [3 Marks]
- Q2. a) Two adjacent edges discontinuous 5 m × 6 m corner slab panel extracted from a sufficiently large slab is shown in the Fig. Q2. Slab is expected to support 5 kN/m² imposed load, self-weight of the deck and load from finishes amounting to 1 kN/m². Take density of concrete as 24 kN/m³ and calculate the critical moments at the continuous and discontinuous edges and in the mid-way of the slab panel. Take the thickness of the slab as 150 mm and consider load from finishes as dead load. Use BS8110 Table 3.14 for the computation of moment coefficients along with formulae given in clause 3.5.3.4 of the same code. [4 Marks]
- b) Calculate the critical reinforcement requirement at the beam supports and at the middle of the slab panel based on requirement to resist applied bending moment, control crack width, deflection, and satisfy the minimum reinforcement requirement. Take cover to all reinforcement in the major direction of bending as 20mm, $f_{ck} = 30 \text{ N/mm}^2$, $f_{yk} = 500 \text{ N/mm}^2$, and the slab is reinforced with 10 mm diameter high yield steel bars. [4 Marks]
- c) Calculate and show whether adequate shear resistance is provided by the selected slab thickness. Use BS8110 Table 3.15 and clause 3.5.3.7 formulae for the calculation.

- c) Calculate and show whether adequate shear resistance is provided by the selected slab thickness. Use BS8110 Table 3.15 and clause 3.5.3.7 formulae for the calculation. [2 Marks]
- d) Draw the reinforcement details of the slab panel. [2 Marks]

Q3 a) Elastic bending moment diagrams for the critical load combinations described in EC2 are shown in Fig. Q3 a) for the continuous beam ABCD. Considering the bending moment diagram shown in Fig. Q3 a) ii), Fig. Q3 a) iii) and Fig. Q3 a) iv) corresponds to EC2 code recommendations calculate main reinforcement requirement of the beam based on elastic bending moment diagram. Take $f_{ck} = 30 \text{ N/mm}^2$, $f_{yk} = 500 \text{ N/mm}^2$, cross sectional dimension of the beam as 300x650 mm, and the effective depth to tension reinforcement (d) and compression reinforcement (d') as 602.5 mm and 47.5 mm respectively. [5Marks]

b) Shear force diagrams for the same beam ABCD is shown in Fig.3 b). Fig. Q3 b) i), Fig. Q3 b) ii) and Fig. Q3 b) iii) shear force diagram for the critical load combinations described under EC2. Propose a shear reinforcement arrangement for the beam ABCD assuming 8 mm high yield steel are used as shear reinforcement. Take $f_{ck} = 30 \text{ N/mm}^2$, $f_{yk} = 500 \text{ N/mm}^2$, cross sectional dimension of the beam as 300x650 mm, and the effective depth to tension reinforcement (d) and compression reinforcement (d') as 602.5 mm and 47.5 mm respectively. [3 Marks]

c) Check serviceability limit state cracking and deflection performance of the beam ABCD based on deemed to satisfy conditions and propose the final reinforcement arrangement for the beam. [2 Marks]

d) Provide the reinforcement detail for the beam based on answers above showing clearly lap length and anchorage length requirements. (Use separate graph sheet for the reinforcement detail) [2 Marks]

Q4 Plan view, and two cross sections of a ground floor column located in a braced structure is shown in Fig Q4 (a). Column is connected to a moment carrying based at the bottom and monolithically cast beams and slab at the first floor level. The cross section dimensions of the beams connected at the first floor level are 250 mm x500 mm and the slab has a 125 mm thickness. From the frame analysis it is found that the column is subjected to axial load and bending moment about its major axis as shown in the Table Q4 below. Column is square section with dimensions of 300 mm x300 mm. The height of the column from top of foundation to the top of the first floor level is 5.5 m.

Table Q4. Loading details of the column

Axial Load	Moment about major axis (kNm)		Moment about minor axis (kNm)	
	Z-Z Axis of bending		Y-Y Axis of bending	
	Top	Bottom	Top	Bottom
1600 kN	80	-60	60	-40

- a) Calculate the effective length of the column about the major and minor axis and determine its classification in accordance to the guide lines provided in EC2. Consider the stiffness of the foundation identical to the stiffness of the first floor beams ($k_1=k_2$).

[2 Marks]

- b) Based on above classification, applied load and applied initial bending moment, calculate the reinforcement detail for the above column located in the ground floor level. Take concrete as $f_{ck} = 30 \text{ N/mm}^2$, reinforcement grade as $f_{yk} = 500 \text{ N/mm}^2$ and assume d_2/h of the column as 0.1. The relevant column interaction diagram is given in the Fig. Q4 (b).

[6 Marks]

- c) Explain how the calculations would have been changed had the frame been considered was un-brazed.

[4 Marks]

Q5. An internal column $300 \text{ mm} \times 300 \text{ mm}$ carries un-factored dead load of 800 kN and an un-factored imposed load of 400 kN . The ground where the structure is expected to be constructed is estimated to have a bearing capacity of 200 kN/m^2 .

- a) Considering, that the column will be supported by an individual footing, and the connection between column and footing idealized as pinned, select suitable square dimension for the column foundation and a thickness for the footing. (Hint: Initial trial depth (d) for the footing shall be based on $d = 10.5 N^{0.5}$ where d is in mm, N (axial load) is in kN.)

[2 Marks]

- b) Based on the selected foundation detail above, calculate the reinforcement detail for the above foundation based on the bending moment requirement at the critical section. Assume grade 30 concrete and grade 500 high yield steel for construction. Take cover to all reinforcement as 50 mm .

[4 Marks]

- c) Calculate the line shear and punching shear resistance of the pad and check whether the required resistances are provided by the selected dimensions of the foundation in the Q5 a) above.

[5 Marks]

- d) Draw the reinforcement detail for the footing

[1 Mark]

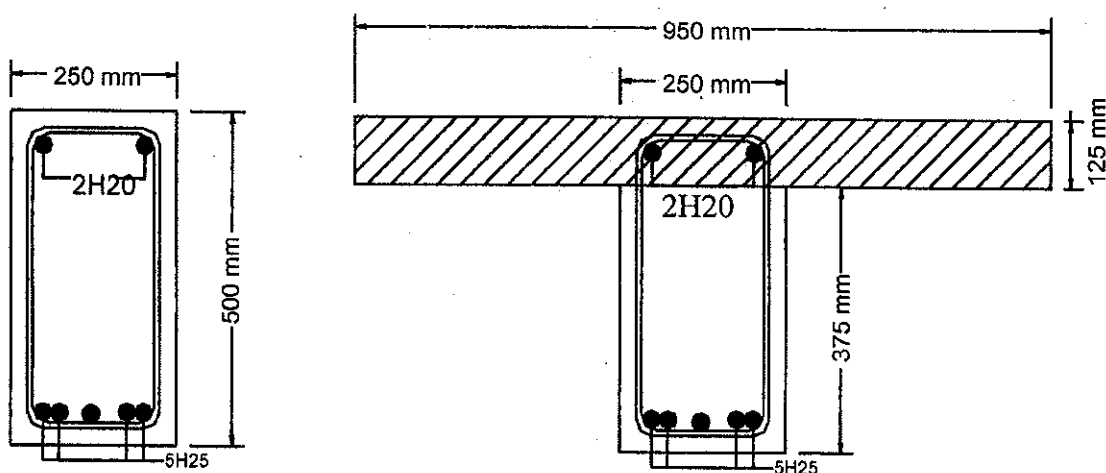


Fig. Q1 a) Rectangular section

Fig. Q1 b) Flange section

Fig. Q1 Rectangular and flange beam section

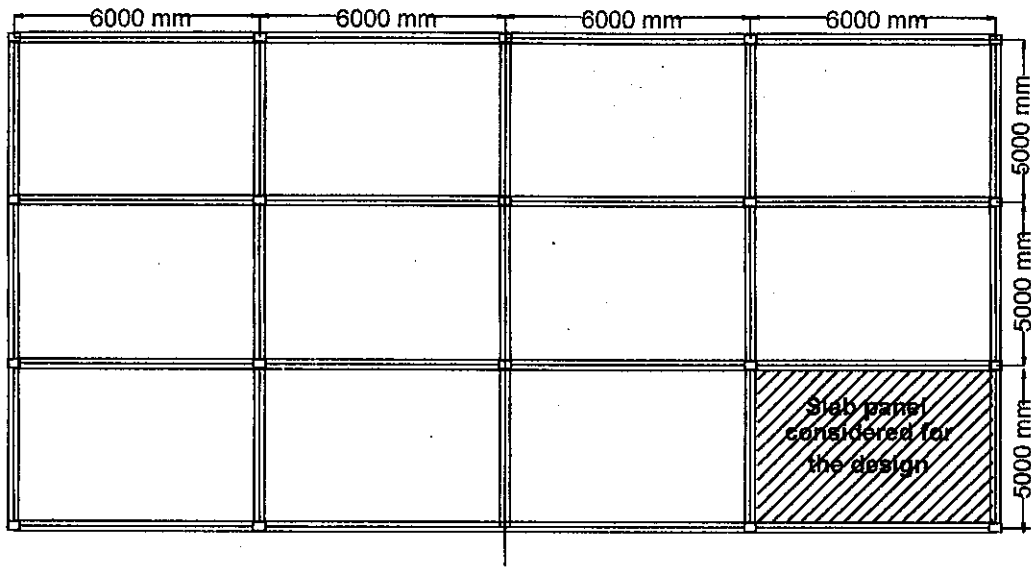


Fig. Q2 Corner slab panel with two adjacent edges discontinuous.

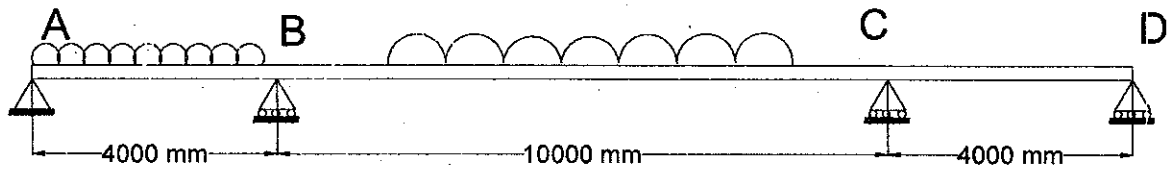


Fig. Q3 a) i) Continuous beam with three spans

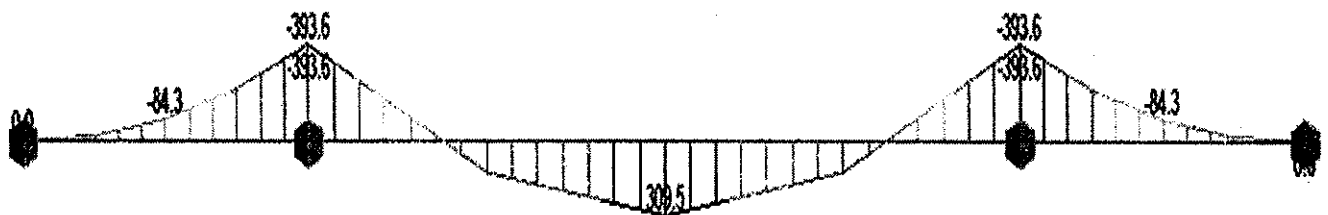


Fig. Q3 a) ii) Case 1: All spans fully loaded

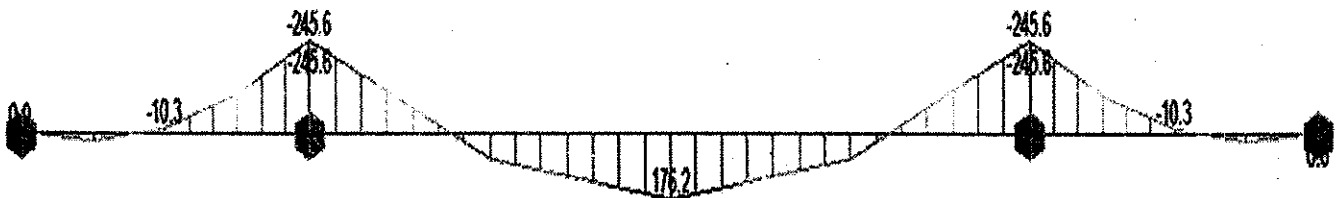


Fig. Q3 a) iii) Case 2: Alternative spans fully loaded maximum loading in the edge two edges

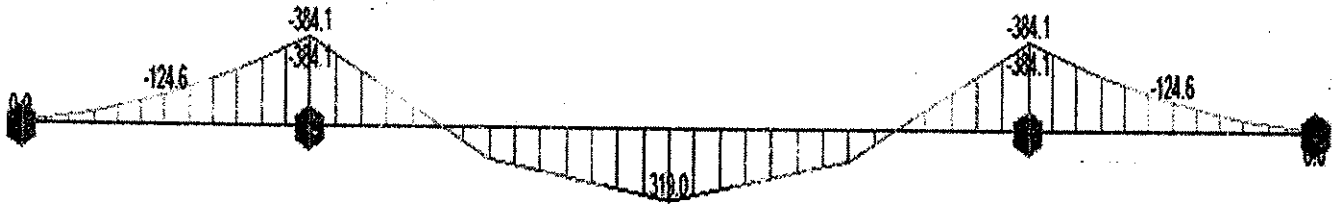


Fig. Q3 a) iv) Case 3: Alternative spans fully loaded maximum loading in the middle span

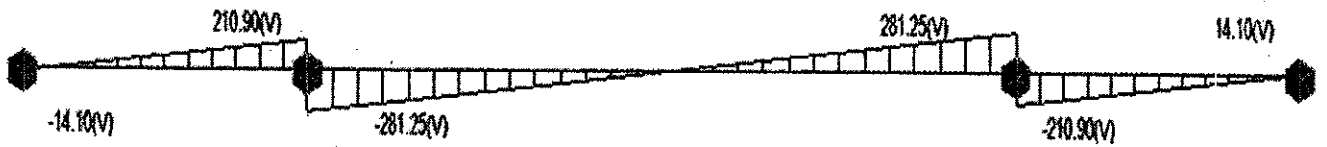


Fig. Q3 b) ii) Case 1: All spans fully loaded



Fig. Q3 b) iii) Case 2: Alternative spans fully loaded maximum loading at the two edges

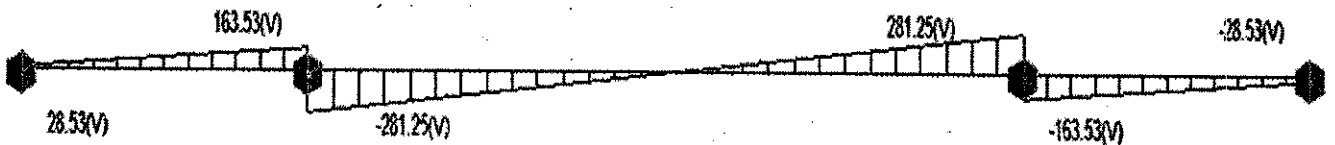
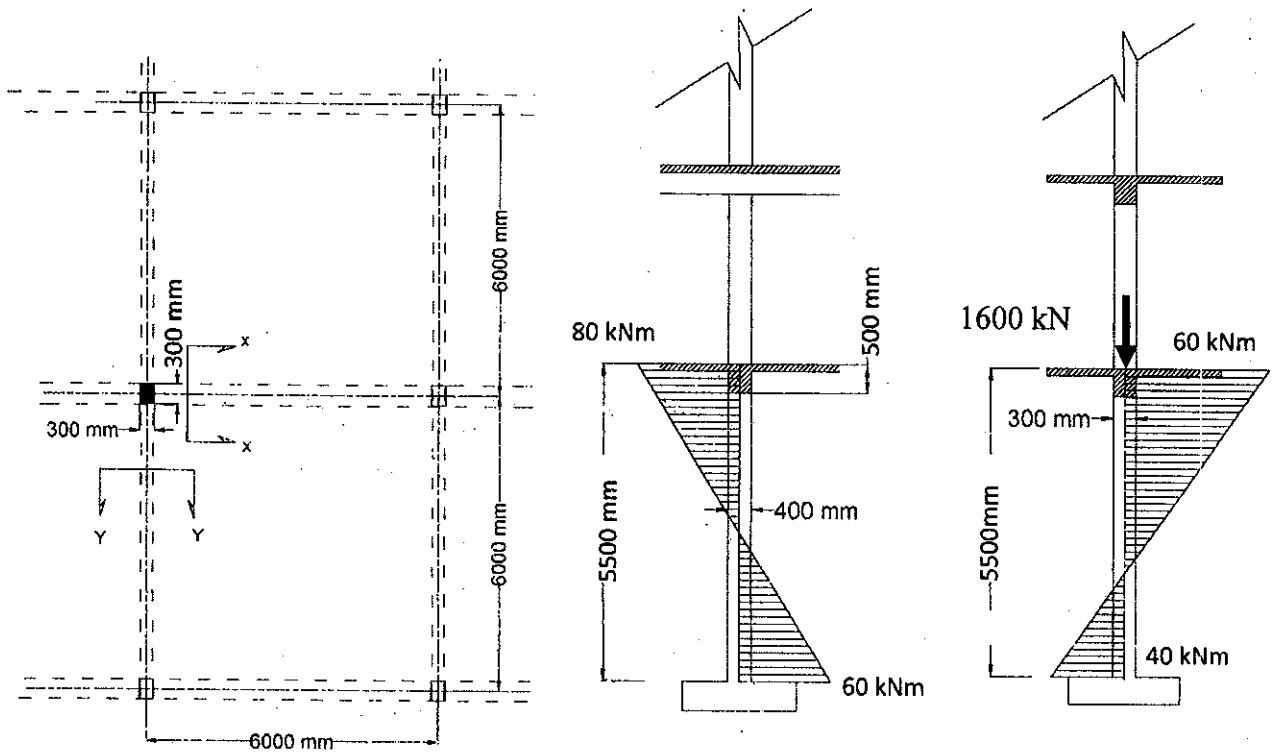


Fig. Q3 a) iv) Case 3: Alternative spans fully loaded maximum loading in the middle span



(i) Plan view

(ii) Section X-X

(iii) Section Y-Y

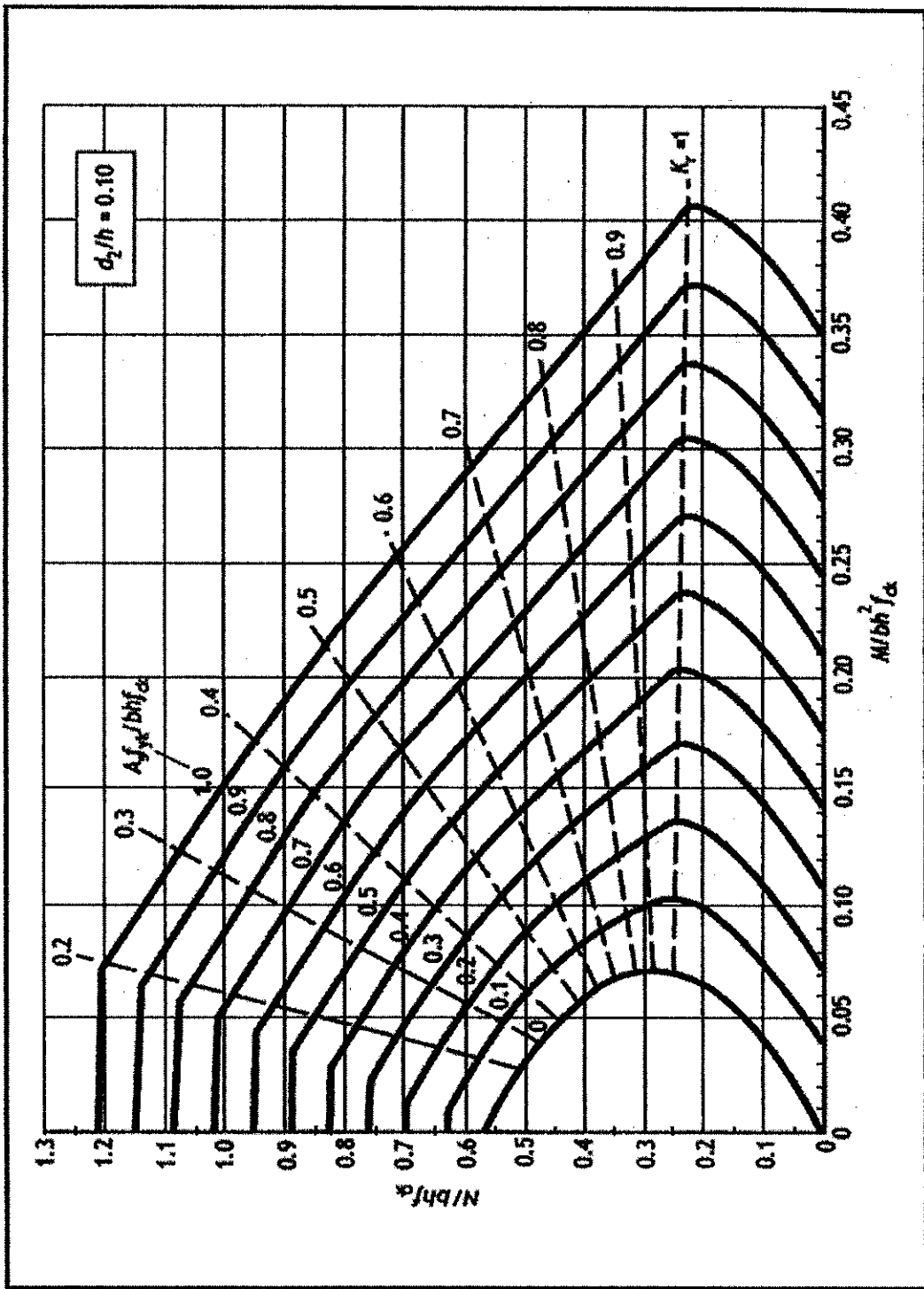


Fig. Q4 b) Relevant column interaction diagram

$$k = \frac{M}{bd^2 f_{ck}}, A_s = \frac{M}{0.87 f_{yk} z}, A'_s = \frac{(k - k') f_{ck} b d^2}{(d - d') 0.87 f_{yk}}, A_s = \frac{0.167 f_{ck} b d^2}{0.87 f_{yk} (d - d')} + A'_s$$

$$z = d \left(0.5 + \sqrt{0.25 - \frac{k}{1.134}} \right), k = \frac{M}{b_f d^2 f_{ck}}, A_s = \frac{M + (0.36d - h_f) 0.1 b_w f_{cu} d}{0.87 \left(d - \frac{h_f}{2} \right) f_y}$$

$$\beta_f = \left(1 - \frac{b_w}{b} \right) \frac{h_f}{d} (0.567) \left(1 - \frac{h_f}{2d} \right) + 0.19 \frac{b_w}{b}, M = \beta_f f_{ck} b d^2$$